Frame 6 Users Conference Phoenix, AZ

June 13, 2006





MS6001 Performance History

Turbine Model	Ship Dates	Firing Temp.	Output*	Heat Rate*	Exh Flow	Exh Temp
		°F/°C	kW	BTU/kWhr	10 x 3lb/hr	°F/°C
MS6431A	1978	1850/1010	31,050	11,220	1,077	891/477
MS6441A	1979	1850/1010	31,800	11,250	1,112	901/483
MS6521B	1981	2020/1104	36,730	11,120	1,117	1017/547
PG6531B	1983	2020/1104	37,300	10,870	1,115	1005/541
PG6541B	1987	2020/1104	38,140	10,900	1,117	999/537
PG6551B	1995	2020/1104	39,120	10,740	1,137	1003/539
PG6561B	1997	2020/1104	39,620	10,740	1,145	989/532
PG6571B**	1997	2077/1136	40,590	10,600	1,160	1005/541
PG6581B	2000	2084/1140	41,460	10,724	1,166	1016/546

*ISO conditions, unit operating at Base Load on Oil Fuel and no inlet or exhaust losses. ** Available as retrofit only

Current New Unit Production



Typical PG6581B vs. PG6541B

PG6581B(new unit)

✓ Stage 1 Shroud	HR-120 Material with 'Pumpkin Tooth'	310 SS with 'Pumpkin
✓ Stage 2 Shroud	Honeycomb Shroud	Non-Honeyc
✓ Stage 3 Shroud	Honeycomb Shroud	Non-Honeyc
✓ Stage 1 Nozzle	FSX-414, Improved Cooled	FSX-414, not Impr
✓ Stage 2 Nozzle	GTD-222 material	FSX-414 ma
✓ Stage 3 Nozzle	GTD-222 material	FSX-414 ma
✓ Stage 1 Bucket	GTD-111, Perimeter, BLE/DS, GT-29 I+	111, 12 hole, BLE/I
✓ Stage 2 Bucket	IN738, 7 hole, cutter tooth design	IN738, 4 hole, non
✓ Stage 3 Bucket	IN738, cutter tooth design	U500, non-cutter to
 ✓ Inlet Guide Vanes angle 	GTD-450 material, 86° maximum angle	403 SS material, 8
✓ Transition Piece TBC	Nimonic -263 Body and aft-frame with TBC	Hast-X body and a
Liner TBC	Standard combustion design with TBC	Standard combusti
Inner Barrel	Standard labyrinth seal design	Standard labyrinth
✓ Load Gear limit	5163 rpm load gear with 51 MW limit	5094 rpm load gea
Firing Temperature	2084°F	2020°F

<u>PG6541B</u>

Tooth' omb Shroud omb Shroud roved Cooled aterial terial

DS, GT-29 I+ n-cutter tooth both design 84° maximum

aft-frame with

ion design w/o

seal design ar with 51 MW



Typical PG6581B vs. PG6551B

PG6581B(new unit)

✓ Stage 1 Shroud	HR-120 Material with 'Pumpkin Tooth'	310 S
✓ Stage 2 Shroud	Honeycomb Shroud	
✓ Stage 3 Shroud	Honeycomb Shroud	
✓ Stage 1 Nozzle	FSX-414, Improved Cooled	FSX
✓ Stage 2 Nozzle	GTD-222 material	
✓ ✓ Stage 3 Nozzle	GTD-222 material	
✓ Stage 1 Bucket	GTD-111, Perimeter, BLE/DS, GT-29 I+	111,
✓ Stage 2 Bucket	IN738, 7 hole, cutter tooth design	IN73
✓ Stage 3 Bucket	IN738, cutter tooth design	U500
✓ Inlet Guide Vanes angle	GTD-450 material, 86° maximum angle	GTD
✓ Transition Piece TBC	Nimonic -263 Body and aft-frame with TBC	Hast
Liner TBC	Standard combustion design with TBC	Stand
Inner Barrel	Standard labyrinth seal design	Stan
 ✓ Load Gear limit 	5163 rpm load gear with 51 MW limit	5094
Firing Temperature	2084°F	2020

PG6551B

SS with 'Pumpkin Tooth' Non-Honeycomb Shroud Non-Honeycomb Shroud -414, not Improved Cooled GTD-222 material GTD-222 material

12 hole, BLE/DS, GT-29 I+ 38, 4 hole, cutter tooth , cutter tooth design -450 material, 86° max.

t-X body N-263aft-frame with

dard combustion design w/o

dard labyrinth seal design 4 rpm load gear with 51 MW

0°F



Typical PG6581B vs. PG6561B

PG6581B(new unit)

✓ Stage 1 Shroud	HR-120 Material with 'Pumpkin Tooth'
✓ Stage 2 Shroud	Honeycomb Shroud
✓ Stage 3 Shroud	Honeycomb Shroud
✓ Stage 1 Nozzle	FSX-414, Improved Cooled
✓ Stage 2 Nozzle	GTD-222 material
✓✓ Stage 3 Nozzle	GTD-222 material
✓ Stage 1 Bucket	GTD-111, Perimeter, BLE/DS, GT-29 I+
✓ Stage 2 Bucket	IN738, 7 hole, cutter tooth design
✓ Stage 3 Bucket	IN738, cutter tooth design
✓ Inlet Guide Vanes	GTD-450 material, 86° maximum angle
angle	
 Transition Piece 	Nimonic -263 Body and aft-frame with TBC
TBC	
Liner	Standard combustion design with TBC
TBC	
Inner Barrel	Standard labyrinth seal design
✓ Load Gear	5163 rpm load gear with 51 MW limit
limit	
Firing Temperature	2084°F

PG6561B

310 SS with 'Pumpkin Tooth' Honeycomb Shroud Honeycomb Shroud FSX-414, not Improved Cooled GTD-222 material GTD-222 material

111, 12 hole, BLE/DS, GT-29 I+ IN738, 6/7 hole, cutter tooth IN738, cutter tooth design GTD-450 material, 86° max.

Hast-X body N-263aft-frame with

Standard combustion design w/o

Standard labyrinth seal design 5133 rpm load gear with 51 MW

2020°F



Wheelspace Temperatures









Fast Start & Black Start Capabilities



BLACK START CAPABILITY

- Diesel start Requires AC power for auxiliaries
- Motor start Requires diesel-generator set

Black start requirements – Diesel start

Auxiliaries requiring AC power must be separately supplied

•Fuel

Gas fuel is available at proper pressure. Otherwise a separate compressor required.

•Ignition Power – Spark Plugs

UPS is normally available for this. Converts battery supplied DC to AC.

•Lube Oil Pumps

DC emergency lube oil pump should be adequate.

•Lube Oil Cooling

Cooling water pumps must be energized.

•Diesel Engine Cooling

Cooling water must be provided to the diesel engine.

•Cooling Water Fans

Power must be supplied to cooling water fans

SCOPE OF SUPPLY (Diesel start)

•UPS system

•Battery system

•Controls modifications

Assumes cooling water system supplied by customer and has adequate power

OR

•A 250KW diesel-generator set with dead bus closure capability to pick up all aux. Power.

•Controls mods



Black start requirements – Motor start

All starting power must be supplied by a separate diesel-generator set with dead bus closure capability. This will require about 1000KW set.



Table 4.1: START SIGNAL TO ISO RATED LOAD E-CLASS SIMPLE CYCLE UNITS										
	Mean Time from Start Signal to FSNL No Purge Time included			Mean Time from FSNL to FSFL (3)						
Starting Device	Starting Time	S tand Dev	Qutoing Limits	Load Time without DLN	Load Time with DLN	Stand Dev	Quoting Limit without	Quoting Limit with DLN	Total Time without DLN	Total Time with DLN
Arthon Participant and			and the second		An Marcalt	37984	2010000			
670 HP Diesel (2300 rpm) (4)	10 min	1 min	12 min	4 min	4 min	1 min	6 min	6 min	16 min	16 min
600 HP Motor	10 min	1 min	12 min	4 min	4 min	1 min	6 min	6 min	14 min	14 min
670 HP Diese) (2300 rpm) (4)	10 min	1 min	12 min	30 sec	2 min	1 min	2 min 30 sec	4 min	12 min 30 sec	14 min
600 HP Motor	10 min	1 min	12 min	30 sec	2 min	1 min	2 min 30 sec	4 min	10 min 30 sec	12 min
		an a	State Carlos and a		Constant of the				2 . 10	0 min 10 mm
570 HP Diesel (1) (4) (2300 rpm)	6 min 40 sec	1 min	8 min 40 sec	30 sec	2 min	1 min	2 min 30 sec	4 min	/ min 40 sec	9 min 10 sec
600 HP Motor (1)	6 min 40 sec	1 min	8 min 40 sec	30 sec	2 min	1 min	2 min 30 sec	4 min	7 min 10 sec	8 min 40 sec
	Starting Device 670 HP Diesel (2300 rpm) (4) 600 HP Motor 670 HP Diesel (2300 rpm) (4) 600 HP Motor 670 HP Diesel (2300 rpm) (4) 600 HP Motor 670 HP Diesel (1) (4) (2300 rpm) 600 HP Motor (1)	TO ISO RATED LOAD E-CLASS SIMPLE CYCLMe an Time FSNL No FStarting DeviceStarting Time670 HP Diesel (2300 rpm) (4)10 min670 HP Diesel (1) (4) (2300 rpm) (4)10 min670 HP Diesel (1) (4) (2300 rpm)6 min 40 sec600 HP Motor (1)6 min 40 sec	TO ISO RATED LOAD E-CLASS SIMPLE CYCLE UNITSMe an Time from St FSNL No Purge TimeStarting DeviceStarting TimeStand Dev670 HP Diesel (2300 rpm) (4)10 min1 min670 HP Diesel (1) (4) (2300 rpm)6 min 40 sec1 min600 HP Motor (1)6 min 40 sec1 min	TO ISO RATED LOAD E-CLASS SIMPLE CYCLE UNITSMe an Time from Start Signal to PSNL No Purge Time includedStarting DeviceStarting TimeStand DevQutoing Limits670 HP Diesel (2300 rpm) (4)10 min1 min12 min670 HP Diesel (1) (4) (2300 rpm)6 min 40 sec1 min8 min 40 sec600 HP Motor (1)6 min 40 sec1 min8 min 40 sec	TO ISO RATED LOAD E-CLASS SIMPLE CYCLE UNITS Me an Time from Start Signal to FSNL No Purge Time included Load Time without Starting Device Starting Time Stand Dev Qutoing Limits Load Time without 670 HP Diesel (2300 rpm) (4) 10 min 1 min 12 min 4 min 670 HP Diesel (2300 rpm) (4) 10 min 1 min 12 min 4 min 670 HP Diesel (2300 rpm) (4) 10 min 1 min 12 min 30 sec 670 HP Diesel (2300 rpm) (4) 10 min 1 min 12 min 30 sec 670 HP Diesel (2300 rpm) (4) 10 min 1 min 12 min 30 sec 600 HP Motor 10 min 1 min 30 sec 30 sec 600 HP Motor 0 min 40 sec 1 min 8 min 40 sec 30 sec 600 HP Motor (1) 6 min 40 sec 1 min 8 min 40 sec 30 sec	IO ISO RATED LOAD E-CLASS SIMPLE CYCLE UNITS Mean Time from Start Signal to FSNL No Purge Time included Mean Time from Start Signal to FSNL No Purge Time included Starting Device Starting Time Stand Dev Qutoing Limits Load Time without Mean Time from Start Signal to FSNL No Purge Time included 670 HP Diesel (2300 rpm) (4) 10 min 1 min 12 min 4 min 4 min 670 HP Diesel (2300 rpm) (4) 10 min 1 min 12 min 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min 4 min 4 min 1 min 6 min 16 min 16 min 670 HP Dissel (2300 rpm) (4) 10 min 1 min 12 min 30 sec 2 min 1 min 6 min 14 min 670 HP Dissel (2300 rpm) (4) 10 min 1 min 12 min 30 sec 2 min 1 min 2 min 30 sec 4 min 1 min 2 min 30 sec 4 min 1 min 10 min 30 sec 4 min 1 min 2 min 30 sec 4 min 1 min 30 sec 4 min 7 min 40 sec 600 HP Motor (1) 6 min 40 sec 1 min 8 min 40 sec 30 sec 2 min 1 min 2 min 30 sec 4 min 7 min 40 sec 600 HP Motor (1) 6 min 40 sec 1 min 8 min 40 sec</td>	IO ISO RATED LOAD E-CLASS SIMPLE CYCLE UNITS Mean Time from Start Signal to FSNL No Purge Time included Mean Time from FSNL to FSFL (3) Starting Device Starting Time Stand Dev Quoting Limits Load Time without DLN Load Time with DLN Stand Dev Quoting Limits Quoting without DLN Quoting without Quoting Limit with DLN Tetal Time without DLN 670 HP Dissel (2300 rpm) (4) 10 min 1 min 12 min 4 min 4 min 1 min 6 min 16 min 16 min 670 HP Dissel (2300 rpm) (4) 10 min 1 min 12 min 30 sec 2 min 1 min 6 min 14 min 670 HP Dissel (2300 rpm) (4) 10 min 1 min 12 min 30 sec 2 min 1 min 2 min 30 sec 4 min 1 min 2 min 30 sec 4 min 1 min 10 min 30 sec 4 min 1 min 2 min 30 sec 4 min 1 min 30 sec 4 min 7 min 40 sec 600 HP Motor (1) 6 min 40 sec 1 min 8 min 40 sec 30 sec 2 min 1 min 2 min 30 sec 4 min 7 min 40 sec 600 HP Motor (1) 6 min 40 sec 1 min 8 min 40 sec



Performance Degradation and Recovery



Performance Degradation and Recovery

- Recoverable and Non-Recoverable
- Degradation of the compressor and turbine
- Degradation <u>factors</u> (fouling, influence coefficients)
- Minimizing performance degradation
- Detection
- Recovery of performance
- Hot Gas Path Audit Services



Expected Gas Turbine Plant Performance Degradation Following Normal Maintenance and Off-Line Compressor Water Wash



Degradation of the Compressor/Turbine

Compressor

- Accounts for 70 85% of power loss •
- Caused by loss in airflow and efficiency
- Results of •
 - Fouling

Erosion

FOD

Rubs

Corrosion

- Recoverable
- Non-recoverable
- Non-recoverable
- Non-recoverable
- Non-recoverable
- Surface rough Recoverable

Turbine

- Loss in efficiency and increased leakage/cooling flows ٠
- Results of •

Rubs

FOD

- Corrosion Erosion
- Non-recoverable
- Non-recoverable
- Non-recoverable
- Non-recoverable



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Compressor Fouling

- Primarily in the front stages (no moisture in rear stages)
- Impacts air flow more than efficiency
- Caused by:
 - Air borne contaminants and availability of moisture
 - dust, sand, salts, hydrocarbons, pollen, insects, industrial chemicals, etc.
 - Humidity, rain, fog, evaporative cooler
 - Other
 - Internal oil leaks
 - Evaporative cooler malfunction
 - Fogger



Minimizing Performance Degradation

Filters

- Addresses erosion problem along with fouling
- Not effective for vapors

Coatings

- Aimed at corrosion problem roughness and fatigue
- Blade profile surface finish trade-off
- Reduced fouling by maintaining smooth finish
- Current GE recommendation
 - GTD 450 IGV plus first three stages
 - GECC-1 coating middle stages
 - 403 stainless uncoated rear stages

Siting

- Wind direction
 - Proximity to coal piles
 - Proximity to steam blowoff (cooling tower plume)
 - Gas turbine exhaust



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Detection

Corrected Power and Heat Rate

- Performance monitor at base load
- Use manufacturers data to adjust for ambient conditions
- Small ratio of heat rate change to power change = airflow loss

Compressor Pressure Ratio (clean fuels)

- Compressor discharge pressure/inlet flange pressure
 - Independent of barometer, inlet system losses
 - Base load, full open IGV, constant ambient and injection
- Direct indicator of compressor airflow (1% pressure ratio = 1% air flow)

Detection (continued)

Compressor Airflow

- Calibrated bellmouth performance monitor package
 - Inlet flange total pressure
 - Annulus static pressure at IGV
 - Compressor inlet temperature
 - Standard equation for flow nozzle
 - Bellmouth flow coefficient from factory test
 Not required for trending
- Must "correct" for ambient conditions



Recovery of Performance

Compressor Washing - GEK 103623A

- Dissolves deposits
- Need to understand nature of fouling detergent
- On-line wash does not interrupt operation, minimal build-up
- Off-line wash more effective more liquid. Use of "hot" water for heavy front end fouling, hand clean first
- Discourage abrasive cleaning on line

Filter Replacement

• Inlet filter plugging -- 4 inches water = at least 1% power

Compressor Cleaning

- Hand scour or solid CO2 blast
 - Mechanical removal of deposits
- Page 24 Casing off procedure

Maintenance Considerations/Clearances



Precision Clearances Taken During Outage

Hot Gas Path (HGP)

- 1. Turbine and Compressor Open 6 Point Clearance
- 2. Turbine Clearance Checks
 - a. First stage nozzle support ring to first stage nozzle segment support pad
 - b. First stage nozzle clamp
 - c. Axial rotor clearances
 - d. Axial seal clearances
 - e. Axial diaphragm to turbine wheel
 - f. Radial seal clearances
 - g. Bucket tip clearance
 - h. Diaphragm radial seal clearance
 - i. Rotor set point
 - j. First stage nozzle support ring shim
 - k. Shroud to bucket clearance
 - I. Axial clearance support ring set dimension
- 3. Rotor Float (Thrust Clearance)
- 4. First stage nozzle radial concentricity check (opening and closing)
- 5. Recheck first stage nozzle radial concentricity check
- 6. Recheck turbine clearance checks
- 7. Verify transition piece side seal clearances and clearance to first stage nozzle
- 8. Turbine and compressor closing 6 point clearances



Precision Clearances Taken During Outage

Major Inspection (MI)

- 1. Initial unit alignment check
- 2. Initial compressor and turbine rotor 6 point clearance
- 3. Rotor thrust check
- 4. Initial compressor half shell clearances
- 5. Turbine clearance check
- 6. First stage nozzle radial concentricity check
- 7. Bearing seal clearance
- 8. Recheck compressor half shell clearances
- 9. Recheck rotor thrust
- 10. Recheck first stage nozzle radial concentricity check
- 11. Recheck turbine clearance checks
- 12. Verify transition piece side seal clearances and clearance to first stage nozzle
- 13. Turbine and compressor closing 6 point clearances
- 14. Recheck unit alignment



Precision Clearances Taken During Outage

At the second major, precision clearances are pretty much impossible due to

- Case distortion
- Foundation shifts
- parts not repaired to spec, etc

Closing clearances need to be evaluated on an individual basis against the next planned outage, history, etc



Compressor Section Recommend Inspections

The following recommendations are for compressor's 2nd, 3rd and 4th major inspections and peak operation units:

Compressor Blades

- Bent Tips
- Airfoil surface for nicks and dents
- Blade rock
- Erosion, Corrosion, and Deposits on the vane
- Pits

Stator Vanes

- •Bent Tips
- Airfoil surface for nicks and dents
- Blade rock
- •Erosion, Corrosion, and Deposits on the vane
- Verify stator rock and stator vane drops.
- Pits

Compressor Casings

- Inspect for cracks in the casing and signs of rubbing.
- Inspect stator vane slots for excess wear and hook fits for damage.

Compressor Section Recommend Inspections

Most critical to watch for are corrosion pits, especially on the 3rd stage stator vanes and on VIGV's (TIL on pitting sizing and location limits)

Check for corrosion/rusting on the back end blades/vanes

Check the wheel rim gaps on four places per stage (if the rotor is not to be removed)

Consider changing out blades/vanes if performance loss is significant

If through bolts are checked (rotor removed/dismantled) and more than 3 need to be replaced, replace the whole set.

If vibrations are creeping up, check the marriage joint and clean it up. Replace the marriage bolt set (do not reuse).



Technical Information Letters – Issued 2005

TIL #	Title	Description				
1275-1R2	Excessive Gas Flow at Start-Up	Inform users of the startup characteristics for gas turbines				
1535-2	6B (PG 6581) Wheelspace TTWS1FI 1-2 Settings	To inform customers the constant WSKALM1 must be changed from 820F (438 C) to 800 F (427 C)				
1537-1	High Gas Flow at Startup - Lratoohy Logic Sequence	To inform users of possible issue with the startup control sequence related to high gas flow protection implemented prior to 2002 and enhanced control sequence that includes a P2 highpressure check during startup and Bottle Check test is available.				
1448-2R2	6B TNHCOR CORRECTED SPEED MODIFICATION	To inform users of a correction factor to the TNHCOR corrected speed value and change the overspeed trip setpoints.				
1505-2	6B EXPANSION JOINT COUPLING MODIFICATION	To advise users that the stop stakes are not installed on some 6B EJC.				
1214-3R3	6B, 6C, 6FA, 6FA+E, 7F, 7FA, 7FA+, 7FA+E, 7FB, 7H, 9F, 9FA, 9FA+, 9FA+E, 9FB, AND 9H bucket lockwire dowel pin assembly procedure and lockwire inspection	Assembly procedure for bucket lockwire dowel pins and recommended inspection of bucket lockwire				
1480-2R1	MARK V FIRMWARE UPGRADE	Mark V firmware upgrade to increase operating reliability of control outputs.				
1518-2	MAINTENANCE AND INSPECTION REQUIREMENTS FOR GAS TURBINE AIR INLET SYSTEM	Explain the required maintenance, inspection and recommendations for the inlet filter compartment, inlet ductwork and plenum.				
1469-2R1	DC EMERGENCY PUMP RECOMMENDATIONS	Recommenations for reliability of the emergency DC pump				
1520-1	HIGH HYDROGEN PURGE RECOMMENDATIONS	Inform users of the risk associated with operating gas turbines with high hydrogen content fuel without protection of a nitrogen purge system.				
1528-3	LUBE OIL VARNISHING	Provides information over the formation of varnish or lacuers within the lube oil system and their effects and information reagrding mitagation technologies.				
1524-3R1	COMBUSTION SPREAD MONITOR UPGRADE FOR MK V AND MK VI	Provide a new and improved combustion monitoring protection software that will enhance the reliability and operation of the gas turbine				